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### AFPTEF REPORT NO. 08-R-02 AFPTEF PROJECT NO. 06-P-105

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Development of the MQ-9 Reaper Propeller Container, CNU-690/E

AFMC LSO/LOP AIR FORCE PACKAGING TECHNOLOGY & ENGINEERING FACILITY WRIGHT PATTERS ON AFB, OH 45433-5540 21 February 2008

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AFPTEF PROJECT NO. 06-P-105

TITLE: Development of the MQ-9 Reaper Propeller Container

### **ABSTRACT**

The Air Force Packaging Technology Engineering Facility (AFPTEF) was tasked with the design of a new shipping and storage container for the MQ-9 Reaper Propeller in March of 2006. The new container is designed to replace the fiber glass container currently used.

The current container provides minimal shock protection and being fiber glass is susceptible to deformation, delamination, and extreme temperatures. Additionally, the fiberglass container can not house the propeller and spinner when the spinner is disassembled, the preferred shipping configuration. AFPTEF used proven design techniques to meet these design requirements.

The CNU-690/E, designed to SAE ARP1967A, is an aluminum, long-life, controlled breathing, reusable shipping and storage container. The new container protects the Propeller mechanically and environmentally. The container passed all qualification tests per ASTM D4169.

The CNU-690/E container not only meets user requirements but also provides an economic saving for the Air Force. The savings will be thousands of dollars per Propeller over the twenty-year life span of the container.

Total man-hours: 1400

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AFPTEF

PUBLICATION DATE:

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#### INTRODUCTION

BACKGROUND – Reaper program office personnel at Wright-Patterson AFB contacted AFPTEF to request the design of a reusable container for the MQ-9 Reaper Propeller that would eliminate current shipping and storage risks. The Reaper Propeller is currently shipped in a fiber glass container. The fiber glass design is susceptible to deformation under constant load and cracking under extreme temperatures, either of which could easily cause a seal failure. Delamination is also a concern if the container is constantly exposed to UV rays, such as sunlight. These factors could lead to a corrosion problem for the propeller. The container supplies little shock protection and can not house the propeller and spinner when disassembled. The Reaper Propeller container is one of a family of new AFPTEF container designs that better protect items during the shipping and storage cycle. Containers were also designed for the Reaper Fuselage, Reaper Wings and Reaper Engine.

<u>REQUIREMENTS</u> – AFPTEF, Program Office personnel and General Atomics agreed upon a list of requirements during initial design discussions. Many of these requirements were not met by the fiberglass container. The requirements are as follows:

- Sealed/controlled-breathing container that protects against varied environmental conditions and weather during either inside or outside shipping and storage
- Propeller shock/vibration limited to 20 Gs
- Reusable and designed for long life (20 years)
- Designed for disassembled Propeller & Spinner
- Low maintenance
- Field repairable hardware
- Forklift capabilities (Base & Cover)
- No loose packing material

### DEVELOPMENT

<u>DESIGN</u> – The Reaper Propeller Shipping and Storage Container (CNU-690/E) design meets all the users' requirements. The CNU-690/E is a sealed, welded aluminum, controlled breathing, reusable container (Appendix 2, Figure 1). The container is engineered for the physical and environmental protection of the Propeller during worldwide transportation and storage. The container consists of a base and a completely removable cover equipped with the special features listed below. The cover is designed to be removed by forklift only (Appendix 2, Figure 2), per the customer's request. Guide posts (Appendix 2, Figure 4) keep the cover from coming in contact with the Engine during cover removal and replacement. The base is a one piece skid/double walled base extrusion with 4-way enclosed forklift openings, humidity indicator, pressure equalizing valve (1.5 psi pressure/ 1.5 psi vacuum), internal document holder and a desiccant port for easy replacement of desiccant (controls dehumidification). A silicone rubber gasket and quick release cam-over-center latches create a water/air-tight seal at the base-cover interface. Container external dimensions are 107.0 inches length, 93.8 inches width, and

36.2 inches height. Container empty weight is 1301 pounds, and 1454 pounds with the propeller in place.

A foam isolation system is integrated into the base and provides shock and vibration protection to 20 G's (Appendix 2, Figure 4). The propeller hub rests on a high density polyethylene load spreader that is integrated into the center foam assembly (Appendix 2, Figure 4). The hole pattern in the load spreader follows the pin pattern on the propeller hub (Appendix 2, Figure 5). The blades "float" over six foam assemblies and are held in place by six heavy duty Velcro straps (Appendix 2, Figure 3). The blades do not rest on the foam assemblies due to static stress loading requirements, but help to prevent damage during loading and unloading. All vibration and impact is mitigated by the center foam assembly. The spinner and its parts are secured in the two spinner parts boxes (Appendix 2, Figures 6 & 7). There are no detachable parts on the container other than the container lid, which eliminates FOD risks.

REAPER ENGINE CONTAINER						
FEATURES						
Pressure Equalizing Valve	2					
Humidity Indicator	1					
Desiccant Port	1					
Internal Document Receptacle	1					
Forkliftable (Base & Cover)	Yes					
Cover Latches	24					
Cover Lift Handles	None					
Cover Lift Rings	None					
Cover Tether Rings	None					
Base Lift Handles	None					
Base Tie-down Rings	8					
Stacking Capability	Yes					

<u>PROTOTYPE</u> – AFPTEF fabricated one CNU-690/E prototype container in house for testing. The prototype container was fabricated in accordance with (IAW) all requirements and tolerances of the container drawing package. The drawing package used for prototype fabrication has been released for the manufacture of production quantities of the container. Each face of the container was uniquely identified for testing identification as shown below.

DESIGNATED	CONTAINER
SIDE	FEATURE
Тор	Cover Top
Aft	Desiccant Port
Right	Right Side from Aft
Left	Left Side from Aft
Forward	Opposite Aft
Bottom	Base Bottom

### **QUALIFICATION TESTING**

<u>TEST LOAD</u> – The test load was a functioning Reaper propeller (Appendix 2, Figure 3). The triaxial accelerometer used to record actual accelerations sustained by the propeller was mounted on the propeller hub (Appendix 2, Figures 8 & 9). The test load weight was 153 pounds.

TEST PLAN – The test plan primary references were ASTM D 4169 and SAE ARP 1967 (Appendix 1). The test methods specified in this test plan constituted the procedure for performing the tests on the container. The performance criteria for evaluation of container acceptability were specified at 20 Gs maximum and an initial and final leak rate of 0.05 psi per hour at 1.5 psi. These tests are commonly applied to special shipping containers providing rough handling protection to sensitive items. The tests were performed at AFPTEF, Building 70, Area C, Wright-Patterson AFB.

<u>ITEM INSTRUMENTATION</u> – The test load was instrumented with a piezoelectric triaxial accelerometer mounted on the propeller hub as close to the center of mass as possible (Appendix 2, Figures 8 & 9). The shape of the propeller and it's orientation in the container resulted in the following accelerometer axis orientations:

X Axis - Directed through container Aft Right corner.

Y Axis - Directed through container Forward Right corner.

Z Axis - Directed through container Top and Bottom sides (Vertical motion).

See Appendix 4 for detailed accelerometer and other instrumentation information.

<u>TEST SEQUENCES</u> – Note: Test sequences were performed at the temperature and humidities described in the test procedure.

### TEST SEQUENCE 1 – <u>Leak Test</u>

<u>Procedure</u> – The desiccant port cover was removed and replaced with a port cover modified for attachment of the digital manometer and vacuum/pressure pump lines. The container was closed and sealed. The leak test was conducted at ambient temperature and pressure. The pneumatic pressure leak technique was used to pressurize the container to a minimum test pressure of 1.5 psi. Maximum allowable leak rate is 0.05 psi per hour. (Appendix 2, Figure 10).

<u>Results</u> – The container passed the leak test with a leak rate less than the maximum allowed rate of 0.05 psi per hour.

### TEST SEQUENCE 2 - <u>Vacuum Retention Test</u>

<u>Procedure</u> – The desiccant port cover was removed and replaced with a port cover modified for attachment of the digital manometer and vacuum/pressure pump lines. The container was closed and sealed. The vacuum retention test was conducted at ambient temperature and pressure. The air inside the container was

evacuated to a minimum vacuum of -1.5 psi. Maximum allowable pressure increase rate is 0.05 psi per hour. (Appendix 2, Figure 10).

<u>Results</u> – The container passed the vacuum retention test with a pressure increase rate less than the maximum allowed rate of 0.05 psi per hour.

### TEST SEQUENCE 3 – Rotational Drops, -40°C (-40°F)

Procedure – The container with the item inside was placed inside an environmental chamber on a 1-inch steel floor and allowed to soak for 24 hours at -40°C; the rotational drops were performed at the end of this soak period. At the customer's request, a drop height of 15 inches (12 inches is the standard drop height for this size container) was used to perform two diagonally opposite corner drops (Aft-right and Forward-left) and two adjacent bottom edge drops (Aft and Left) onto the steel chamber floor, and the impact levels were recorded. The maximum allowed impact level for the item was 20 Gs. (Appendix 2, Figure 11)

Results – Three of the recorded resultant G data impact peaks exceeded the maximum allowable 20 Gs. The aft bottom edge, the aft-right corner and the forward-left corner had resultant Gs of 24, 21 and 24 respectively. Due to the use of foam cushioning, these were the lowest achievable impact levels that could be achieved. The propeller was carefully examined after testing by the manufacturer and no damage was found. These G-levels are therefore deemed acceptable.

There was no damage to either the container or the item as a result of the testing. The container met the test requirements. (Appendix 3, Table 1 and Waveforms.)

### TEST SEQUENCE 4 – Rotational Drops, +60°C (+140°F)

<u>Procedure</u> – The container was allowed to soak in the same environmental chamber for 24 hours at +60°C; Test Sequence 1 was repeated at the end of this soak period on the two unimpacted corners (Aft-left and Forward-right) and bottom edges (Forward and Right). (Appendix 2, Figure 12)

<u>Results</u> – All of the recorded resultant impact peak G data was equal to or less than the maximum allowed 20 Gs. There was no damage to either the container or the item as a result of the testing. The container met the test requirements. (Appendix 3, Table 1 and Waveforms.)

### TEST SEQUENCE 5 – <u>Lateral Impact (Pendulum Impact)</u>, -40°C (-40°F)

<u>Procedure</u> – The container was allowed to soak in the environmental chamber at -45°C for 24 hours (a lower soak temperature was used to ensure that the contents would remain as close as possible to the required test temperature throughout impact testing). At the end of the soak period, the container was removed from the chamber, quickly moved to the pendulum test apparatus and impacted once on two adjacent sides (Aft and Right). The container impact velocity was 7.3 ft/s. (Appendix 2, Figure 13)

<u>Results</u> – All recorded resultant impact peak G data were equal to or less than the maximum allowed 20 Gs. There was no damage to either the container or the item. The container met the test requirements. (Appendix 3, Table 1 and Waveforms.)

### TEST SEQUENCE 6 – <u>Lateral Impact (Pendulum Impact)</u>, +60°C (+140°F)

Procedure – The container was allowed to soak in the environmental chamber at +65℃ for 24 hours (a higher soak temperature was used to ensure that the contents would remain as close as possible to the required test temperature throughout impact testing). At the end of the soak period, the container was removed from the chamber, quickly moved to the pendulum test apparatus and impacted once on two unimpacted adjacent sides (Forward and Left). The container impact velocity was 7.3 ft/s. (Appendix 2, Figure 14)

<u>Results</u> – All recorded resultant impact peak G data were equal to or less than the maximum allowed 20 Gs. There was no damage to either the container or the item. The container met the test requirements. (Appendix 3, Table 1 and Waveforms.)

### TEST SEQUENCE 7 - Leak Test

<u>Procedure</u> – Test Sequence 1 was repeated.

<u>Results</u> – The container passed the leak test with a leak rate less than the maximum allowed rate of 0.05 psi per hour.

### TEST SEQUENCE 8 - Vacuum Retention Test

<u>Procedure</u> – Test Sequence 2 was repeated.

<u>Results</u> – The container passed the vacuum retention test with a pressure increase rate less than the maximum allowed rate of 0.05 psi per hour.

<u>TEST CONCLUSIONS</u> – No damage occurred during the above testing to the container, foam isolation system or test item. All impact levels are at or below the item fragility limit of 20 Gs, with the exceptions explained above. Therefore, the container and mounting system do provide adequate protection for the propeller.

### FIT & FUNCTION TESTING

Fit and function testing was completed on site at AFPTEF with the Reaper Propeller that was supplied for prototype testing.

### **CONCLUSIONS**

No damage occurred during the above testing to the container, cushioning system or test item. All impact levels are below the item fragility limit of 20 G's with the exceptions of the occurrences outlined above. The CNU-690/E aluminum container was accepted by the Predator Program Office at Wright-Patterson AFB. The container met all the user's requirements. The container can protect a Reaper Propeller during world-wide transportation and storage and will save the Air Force tens of thousands of dollars in O&M costs. In addition the containers now meet program rapid deployment and operational requirements.

#### RECOMMENDATIONS

AFPTEF recommends that new containers be procured and delivered to avoid damage to Reaper Propellers currently in the logistics cycle, thus mitigating overall shipping risks. All fiberglass containers for the Reaper Engine should be replaced.

**APPENDIX 1: Test Plan** 

AF P	ACKAGINO	G TECH	INOLOG	Y AND EN	NGINEE	RING FACILI	TY AFPTEF PROJECT	NUM BER:
	(Container Test Plan)						06-P-105	
	INER SIZE (L x \	V x D) EXTE	RIOR ·	WEIG GROSS:	HT ITEM:	C UBE (CU.F)	QUANTITY:	DATE:
	x 93.3 x 31.2		93.8 x 36.2	1454	153	209.8	1	October 06
ITEM N			ı	1				
	Reaper P	ropeller						
	ner name: sable Shipp	ina & St	orage Con	ntainer			CONTAINER COST	:
	ESCRIPTION:	ing & Ot	orage our	itanici				
		num Con	ıtainer, Te	st Load of	a MQ-9 F	Reaper Propel	ler	
	noning: oted below							
	REF STD/S	PEC						
TEST NO.	AND TEST MET PROCEDURE	HOD OR	٦	TEST TITLE ANI	D P AR AMETE	RS	CONTAINER ORIENTATION	INSTRU- MENTATION
				<u>N</u> 0	<u>OTE</u>			
			Package		serviceable			
			<u>Qua</u>	lity Confe	ormance	e Tests		
1.	<u>Examinati</u>	on of P	roduct.					
	SAE ARP Par. 4.5.1 Table I	1967	determine workman	r shall be ca e conforman ship, and re in Table an	nce with mequire ment	naterial, es as	Ambient temp.	Visual Inspection (VI)
2.	Weight To SAE ARP Par. 4.5.8.	1967	Container	shall be we	eighed.		Ambient temp.	Scale
			<u>P</u>	<u>erformar</u>	nce Test	<u>s</u>		
3.	Leak Tes	t.						
<b>J.</b>	SAE ARP Par. 4.5.2		retention stabilizati	c pressure a at 1.5 psi. A on, pressure er hour. Pe et series.	After temp e drop shal	Ambient temp.	Water Manometer (WM) or Pressure Transducer (PT)	
СОММЕ	NTS:		1					ı
	RED BY:					APPROVED BY:		
Joel	A. Sullivan,	Mechar	nıcal Engir	neer		Robbin L.	Miller, Chief AFPT	EF

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AF P	ACKAGING TECH				RING FACIL	ITY	AFPTEF PROJECT NU	M BER:
	(Container Test Plan)						06-P-105	
	INER SIZE (L x W x D) ERIOR: EXTE	RIOR:	WEIGH GROSS:	HT ITEM:	CUBE (CU.F)		QUANTITY:	DATE:
106.5	x 93.3 x 31.2					1	October 06	
ITEM N					MANUFACTURER:			
	Reaper Propeller							
	ner name: sable Shipping & St	orage Con	tainer				CONTAINER COST:	
	ESCRIPTION:	orage con	itanici					
Extru	ded Aluminum Cor	tainer, Te	st Load of	a MQ-9 F	leaper Propel	ller		
	ioning: oted below							
TEST NO.	REF STD/SPEC AND TEST METHOD OR PROCEDURE NO'S	1	EST TITLE AND	D P AR AMETE	RS		CONTAINER ORIENTATION	INSTRU- MENTATION
4.	Rotational Drop 3	ests (Low	/ Tempera	ture).				
	SAE ARP 1967 Par. 4.5.3 ASTM D 4169 ASTM D 6179 Methods A&B	4332 for 2		op height	W ASTM D shall be 15". 20G's.	botto drop:	drop on diagonal om corners (2 s) and one drop djacent edges (2 s).*	VI Tri-axial Accelerometer
5.	Rotational Drop 3	ests (Hig	h Tempera	ature).				
	SAE ARP 1967 Par. 4.5.3 ASTM D 4169 ASTM D 6179 Methods A&B	D 4332 fc	or 24 hours.	Drop heig	AW ASTM ght shall be e than 20G's.	botte drop on a	drop on dia gonal om corners (2 ss) and one drop dja cent edges (2 ss).**	VI Tri-axial Accelerometer
6.	Lateral Impact To	est (Low T	- emperatu	ıre).				
	SAE ARP 1967 Par. 4.5.6 ASTM D 4169 ASTM D 880 Procedure B	24 hours.	at -54°C IA Impact velo ustain more	ocity 7.3 ft	/s. Item	end	impact on an and one on a (2 impacts).*	VI and Tri-axial Accelerometer
COMME	NTS: *Thomas duran	ond iver-	oto ove	masiks H	0000 mode	) od :	a toot E 9 7	
COMME	**These drops **This drop is	and impa opposite t	cts are op that perfoi	pposite th rmed in t	iose perform est 4.	ied i r	niesī5 & /.	
PREPAR					APPROVED BY:			
Joel	A. Sullivan, Mechai	nical Engin		Robbin L.	Mille	r, Chief AFPTEF	-	

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ΔFP	ACKAGIN(	G TECH	INOLOG	V AND FI	NGINEE	RING FACILI	пγ	AFPTEF PROJECT NU	JMBER:
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CONT	AINER SIZE (L x V			WEIGI		C UBE (CU.F)	$\dashv$	QUANTITY:	DATE:
INT	ERIOR:	EXTE	RIOR:	GROSS:	ITEM:				
	x 93.3 x 312	107.0 x	93.8 x 36.2	1454	153	209.8		1	October 06
ITEM N		محالح ددد			ı	MANUFACTURER:			
	9 Reaper Pr	ropeller					—	CONTAINER COST:	
	aner name: sable Shippi	ina & St	orana Cor	ntainar				CONTAINER COST.	
	ESCRIPTION:	ing a ca	orage con	laniei					
Extr	uded Alumir	num Cor	ntainer, Te	st Load of	a MQ-9 F	Reaper Propell	ler		
	FIONING:		- ,			1			
As n	oted below								
TEST NO.	R EF STD/S AND TEST MET PROCEDURE	THOD OR	1	TEST TITLE AND	D PARAMETE	:RS		CONTAINER ORIENTATION	INSTRU- MENTATION
7.	Lateral Im	pact Te	st (High T	<u>Γemperatu</u>	<u>ıre)</u> .				
	SAE ARP 1 Par. 4.5.6 ASTM D 4 ASTM D 8 Procedure	1169 380	24 hours.	n at +74°C IA Impact velo sustain more	locity 7.3 f		end	e impact on an d and one on a e (2 impacts).**	VI and Tri-axial Accelerometer
8.	Leak Test								
СОММІ	SAE ARP Par. 4.5.2		retention a stabilization 0.05 psi per end of test	er hour. Per t series.	After tempe e drop shall r form leak	erature I not exceed test again at	Ai	mbient temp.	Water Manometer (WM) or Pressure Transducer (PT)
	THE	Прасс	ю оррос	.o mar pe.	10111100.	11 1001 0.			
PREPAR	RED BY:					APPROVED BY:			
. റല	A. Sullivan.	Mechar	oical Engir	neer		Bobbin I	Mille	er. Chief AFPTE	=

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**APPENDIX 2: Fabrication & Testing Photographs** 

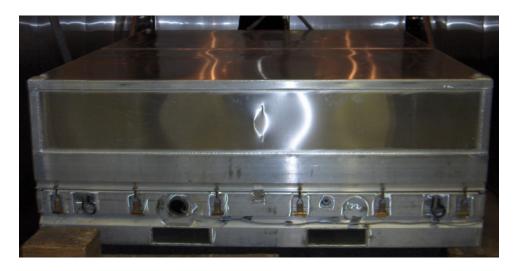


Figure 1. Closed Container.



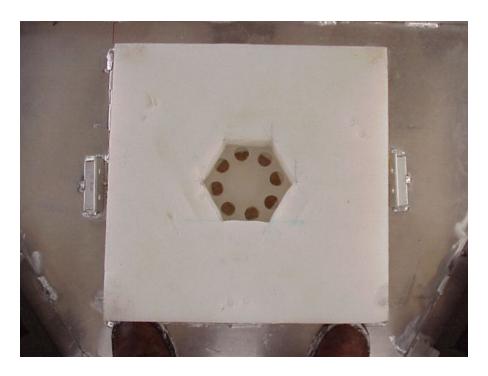
Figure 2. Container cover with enclosed fork tubes.



**Figure 3.** Propeller in container base. (See Figure 4 for current foam configuration)



**Figure 4.** Approved Isolation Assembly Configuration.



**Figure 5.** Center Foam Assembly.



**Figure 6.** Large Spinner Parts Box.



Figure 7. Small Spinner Parts Box.

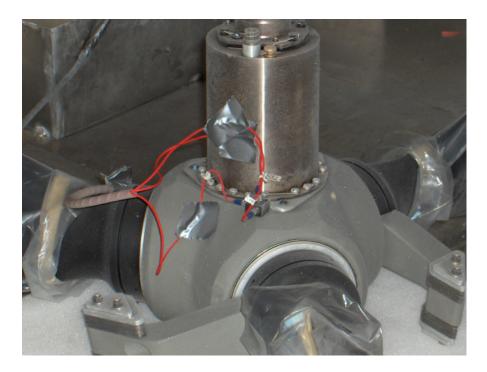


Figure 8. Placement of accelerometer on center propeller housing.



**Figure 9.** Orientation of accelerometer on propeller in container.



**Figure 10.** Pressure Test Set-up (for both pressure and vacuum).



**Figure 11.** Rotational Corner Drop (-40°C).



**Figure 12.** Rotational Edge Drop  $(+60^{\circ}C)$ .



**Figure 13.** Pendulum Impact Test (-40°C).



**Figure 14.** Pendulum Impact Test  $(+60^{\circ}C)$ .

**APPENDIX 3: Test Data** 

 Table 1. Reaper Propeller Impact Test Summary

IMPACT TYPE	TEST TEMPERATURE	IMPACT LOCATION	RESULTANT PEAK G
ROTATIONAL - EDGE	-40°F	aft-bottom	24
ROTATIONAL - EDGE	-40°F	left-bottom	19
ROTATIONAL - CORNER	-40°F	aft-right	21
ROTATIONAL - CORNER	-40°F	forward-left	24
ROTATIONAL - EDGE	+140°F	forward-bottom	15
ROTATIONAL - EDGE	+140°F	right-bottom	15
ROTATIONAL - CORNER	+140°F	aft-left	15
ROTATIONAL - CORNER	+140°F	forward-right	20
LATERAL IMPACT - FACE	-40°F	aft	13
LATERAL IMPACT - FACE	-40°F	right	10
LATERAL IMPACT - FACE	+140°F	forward	19
LATERAL IMPACT - FACE	+140°F	left	20

#### ROTATIONAL DROP TEST

Time:

Oct 6 2006 9:28

Test Engineer:

Evans

Test Type:

Edge, -40°F

Impact Point:

Aft bottom edge

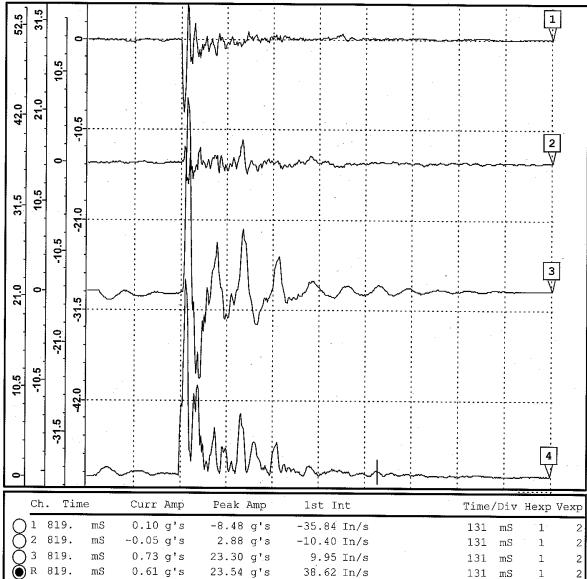
Container/Item:

Aluminum/Propeller

Drop Height:

15 inches

V. Angle: 82.21; H. Angle: 94.21;



Remarks

Peak Gs X: 8 Y: 3 Z: 23 Peak Gs Resultant: 24

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert).
Ch.4=Resultant.

### Propeller Reaper

#### ROTATIONAL DROP TEST

Time:

Oct 6 2006 10:02

Test Engineer:

Evans

Test Type:

Edge, -40°F

Impact Point:

Left bottom edge

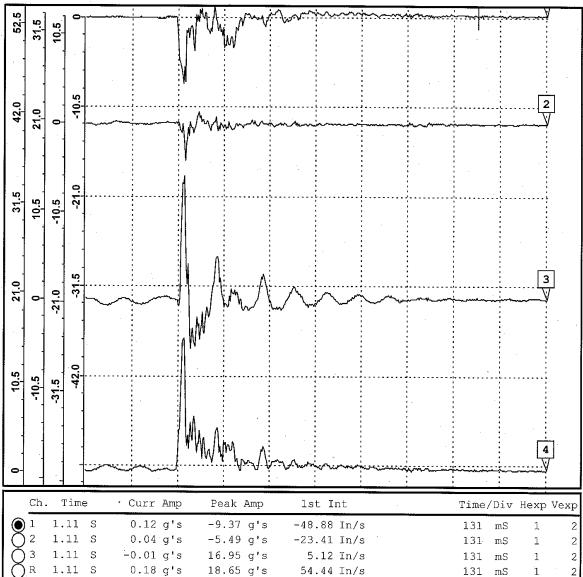
1

mS

Container/Item: Aluminum/Propeller Drop Height:

15 inches

V. Angle: 20.03; H. Angle: 340.43;



Remarks

Peak G X: 9 Y: 5

Z(vert): 17 Peak G Resultant: 19

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner; Ch.3=Z(vert). Ch.4=Resultant.

#### ROTATIONAL DROP TEST

Time:

Oct 6 2006 9:19

Test Engineer:

Evans

Test Type:

Corner, -40°F

Impact Point:

Aft right corner

131 mS

131 mS

1

1

2

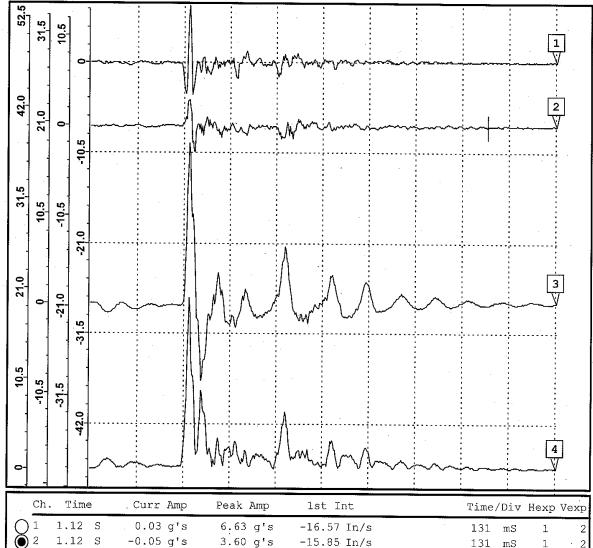
2

Container/Item: Aluminum/Propeller

Drop Height:

15 inches

V. Angle: 83.40; H. Angle: 257.73;



Remarks

1.12 S

1.12 S

Peak Gs X: 7 Y: 4 Z: 19 Peak Gs Resultant: 21

-0.24 g's

0.25 g's

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert).
Ch.4=Resultant.

19.23 g's

20.52 g's

Aft Side = desiccant port side.
ASTM D4169, ASTM D6179. SAE ARP 1967. Accelerometer S/N 16471.

3.87 In/s

23.25 In/s

### ROTATIONAL DROPS TEST

Time:

Oct 6 2006 9:37

Test Engineer:

Evans

Test Type:

Corner, -40°F

Impact Point:

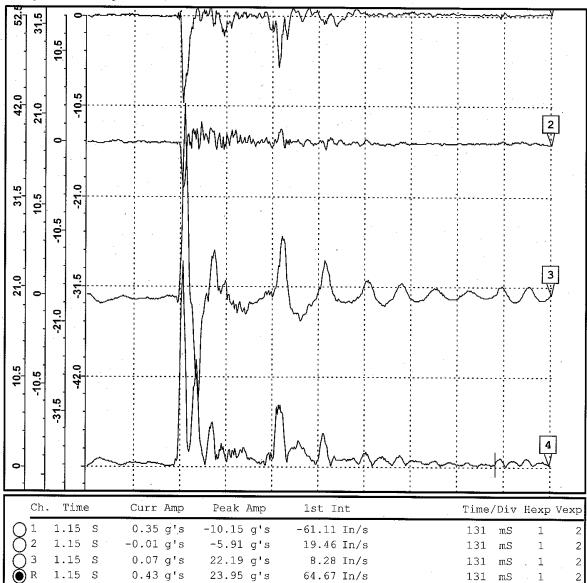
Forward left corner

Container/Item: Aluminum/Propeller

Drop Height:

15 inches

V. Angle: 12.01; H. Angle: 94.29;



Remarks

Peak Gs X: 10 Y: 6 Z: 22 Peak Gs Resultant: 24

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert).
Ch.4=Resultant.

### ROTATIONAL DROP TEST

Time:

Oct 10 2006 9:40

Test Engineer:

Evans

15 inches

Test Type:

Container/Item:

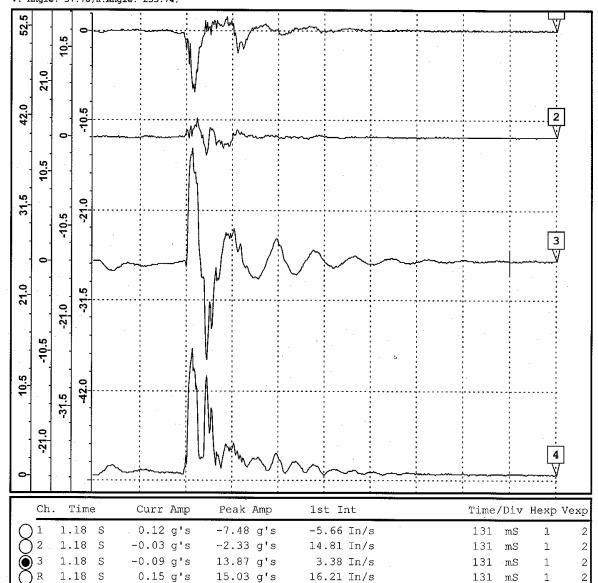
Edge, +140°F

Impact Point:

Forward bottom edge

Aluminum/Propeller Drop Height:

V. Angle: 37.78; H. Angle: 253.74;



Remarks

Peak Gs X: 7 Y: 2 Z: 14 Peak Gs Resultant: 15

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert).
Ch.4=Resultant.

### ROTATIONAL DROP TEST

Time:

Oct 11 2006 12:50

Test Engineer:

Evans

Test Type:

Edge, +140°F

Impact Point:

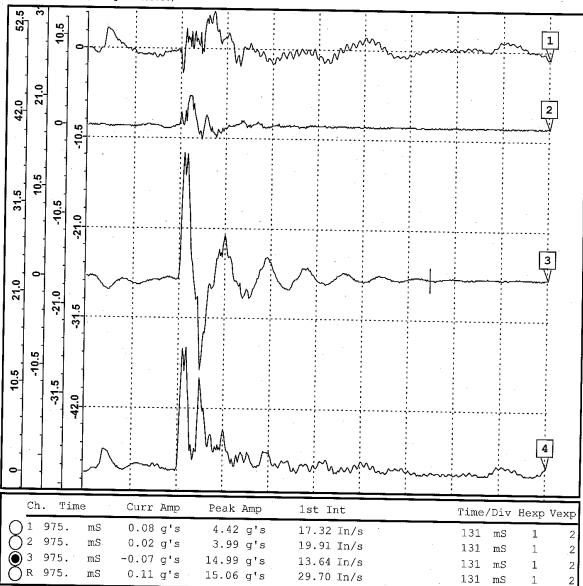
Right bottom edge

Container/Item: Aluminum/Propeller

Drop Height:

15 inches

V. Angle: 41.84; H. Angle: 285.64;



Remarks

Peak G X: 4

Y: 4

Z(vert): 15

Peak G Resultant: 15

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert).
Ch.4=Resultant.

### ROTATIONAL DROP TEST

Time:

Oct 10 2006 9:27

Test Engineer:

Evans

Test Type:

Corner, +140°F

Impact Point:

Aft left corner

2

131

mS

1

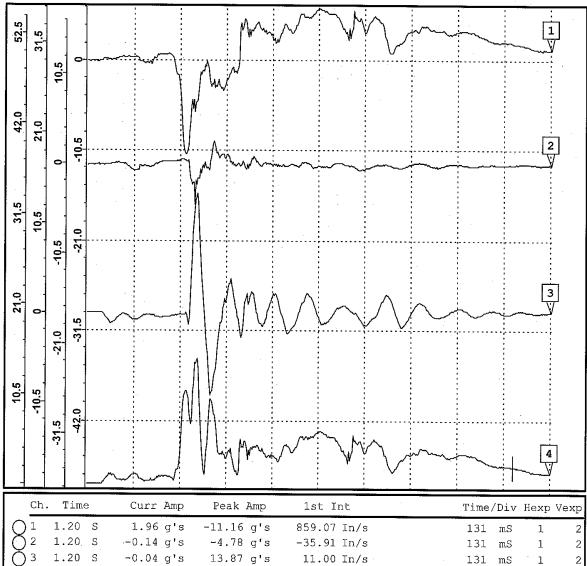
Container/Item:

Aluminum/Propeller

Drop Height:

15 inches

V. Angle: 4.34; H. Angle: 196.09;



Remarks

R

1.20 S

Peak G X: 11 Y: 5 Z(vert): 14

1.91 g's

Peak G Resultant: 15

859.89 In/s

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert).
Ch.4=Resultant.

14.82 g's

#### ROTATIONAL DROP TEST

Time:

Oct 10 2006 9:37

Test Engineer:

Evans

Test Type:
Container/Item:

Corner, +140°F

Aluminum/Propeller

Impact Point:

Forward right corner

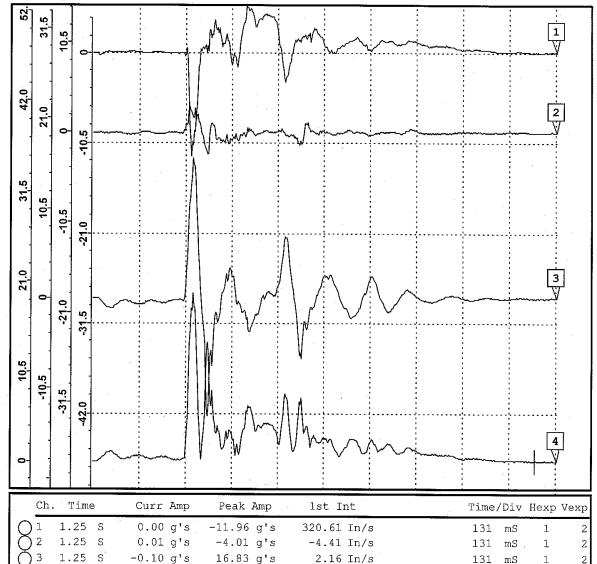
131 ms

2

1

Drop Height: 15 inches

V. Angle: 87.80; H. Angle: 274.40;



Remarks

R

1.25 S

Peak Gs X: 12 Y: 4 Z: 17 Peak Gs Resultant: 20

0.10 g's

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert).
Ch.4=Resultant.

20.17 g's

Aft Side = desiccant port side.
ASTM D4169, ASTM D6179. SAE ARP 1967. Accelerometer S/N 16471.

320.65 In/s

2

2

131

131 mS

mS

1

1

## Reaper Propeller

#### PENDULUM IMPACT TEST

Time:

Oct 19 2006 14:00

Test Engineer:

Evans

Test Type:

Side, -40°F

Impact Point:

Aft side

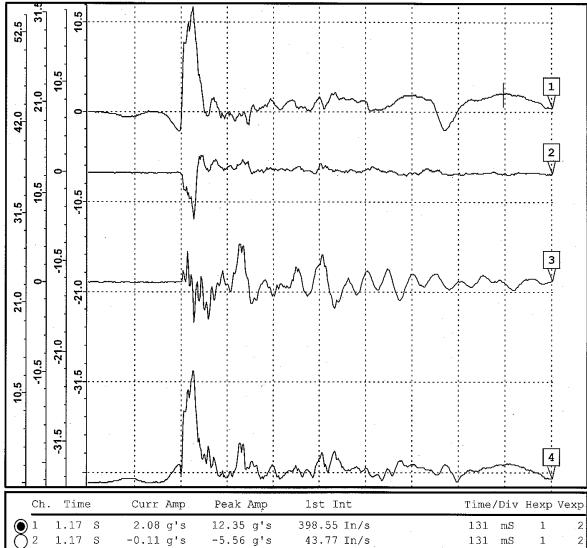
Container/Item:

Aluminum/Propeller

Impact Velocity

7.3 ft/s

V. Angle: 3.14; H. Angle: 164.18;



Remarks

3

1.17 S

S

1.17

Peak Gs X: 12 Peak Gs Resultant: 13

0.03 g's

2.09 g's

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert). Ch.4=Resultant.

-5.09 q's

13.18 g's

Aft Side = desiccant port side. ASTM D4169, ASTM D6179. SAE ARP 1967. Accelerometer S/N 16471.

-50.49 In/s

404.12 In/s

#### PENDULUM IMPACT TEST

Time: Test Type: Oct 19 2006 13:53 Side impact, -40°F Test Engineer: Impact Point: Evans Right side

131 mS

131

131

131 mS

mS

mS

1

1

1

1

2

2

2

2

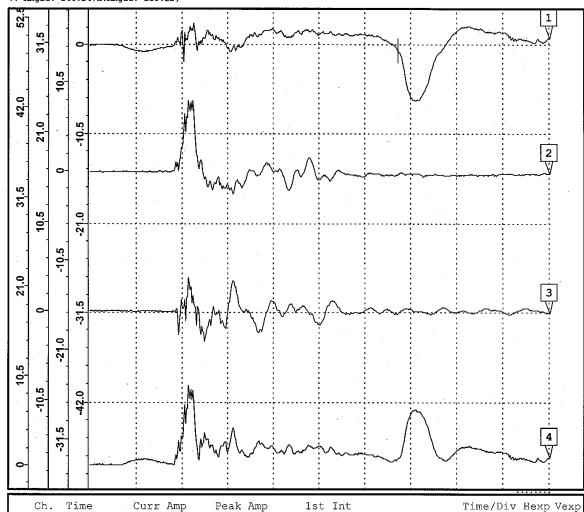
Container/Item:

Aluminum/Propeller

Impact Velocity

7.3 ft/s

V. Angle: 146.24; H. Angle: 219.32;



Remarks

3 878.

1 878.

2 878.

R 878.

mS

mS

mS

mS

Peak Gs X: 7 Y: 9 Z: 4 Peak Gs Resultant: 10

-0.62 g's

-0.32 g's

-0.26 g's

0.74 g's

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert).
Ch.4=Resultant.

3.39 g's

8.55 g's

4.09 g's

9.58 g's

Aft Side = desiccant port side.
ASTM D4169, ASTM D6179. SAE ARP 1967. Accelerometer S/N 16471.

223.71 In/s

13.14 In/s

-27.61 In/s

225.79 In/s

#### PENDULUM IMPACT TEST

Time:

Oct 13 2006 13:10

Test Engineer:

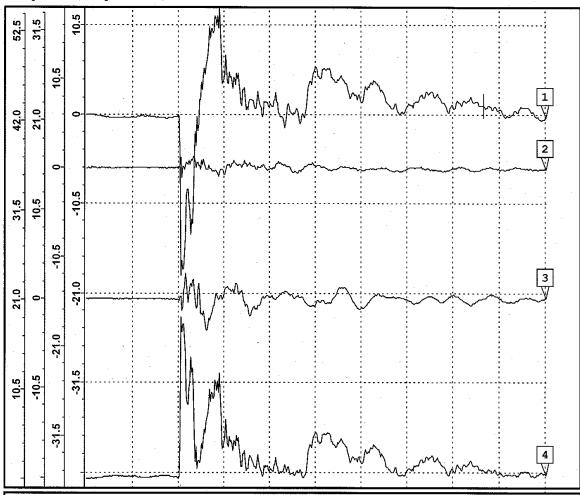
Evans

Test Type: Container/Item: Side impact, +140°F Aluminum/Propeller

Impact Point:

Forward side Impact Velocity 7.3 ft/sec

V. Angle: 1.38; H. Angle: 164.36;



Ch	. Time	Curr Amp	Peak Amp	1st Int	Time/Div Hexp Vexp
1	1.13 S	0.99 g's	-19.22 g's	549.69 In/s	131 mS 1 2
$O^2$	1.13 S	-0.02 g's	1.65 g's	3.94 In/s	131 mS 1 2
ŎЗ	1.13 S	0.01 g's	-3.88 g's	-9.29  In/s	131 mS 1 2
O R	1.13 S	0.99 g's	19.22 g's	549.78 In/s	131 ms 1 2

Remarks

Peak G X: 19

Y: 2

Z(vert): 4

Peak G Resultant: 19

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert). Ch.4=Resultant.

Aft Side = desiccant port side.

ASTM D4169, ASTM D6179. SAE ARP 1967. Accelerometer S/N 16471.

### PENDULUM IMPACT TEST

Time: Test Type: Oct 11 2006 13:35

Test Engineer:

Evans Left side

Container/Item:

Side impact, +140°F

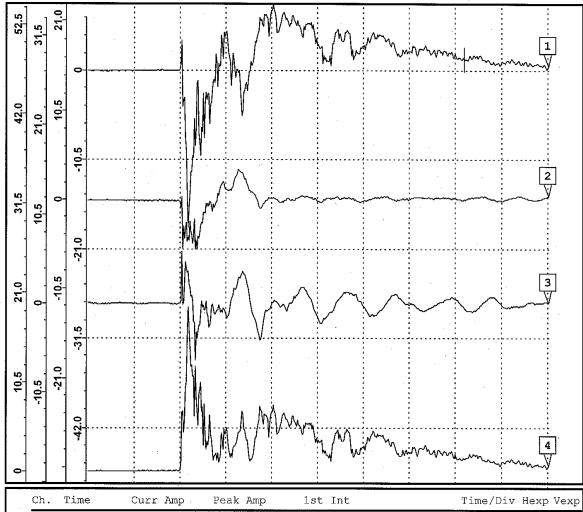
Impact Point:

Aluminum/Propeller

Impact Velocity

7.3 ft/s

V. Angle: 22.25; H. Angle: 274.36;



	Ch.	Time	Cu	rr	Amp	Peak	c A	mp	 1st 1	Int	•	Time	/Div	Нехр	Vexp
(	) 1	1.07	3 1.	.33	g's	-18.7	3 (	g's	592.60	In/s		131	mS	1	2
$I \subset$	2	1.07 \$	0.	04	g's	-9.6	1 0	g's	-0.08	In/s		131	mS	1	2
ΙČ		1.07		54	g's	-6.6	7 (	g's	-37.37	/ In/s		131	mS	. 1	2
IC	R	1.07 5	1.	43	g's	19.7	5 (	g's	593.78	] In/s		131	mS	1	2

Remarks

Peak Gs X: 19 z: 7 Peak Gs Resultant: 20 Y: 10

Ch.1=X(aft, right corner); Ch.2=Y(right, frwd corner); Ch.3=Z(vert). Ch.4=Resultant.

Aft Side = desiccant port side.

ASTM D4169, ASTM D6179. SAE ARP 1967. Accelerometer S/N 16471.

## **APPENDIX 4: Test Instrumentation**

## PRESSURE TEST EQUIPMENT - Test sequences 1, 2, 7 & 8

EQ UIPMENT	MANUFACTURER	MODEL	SN	CAL. DATE
Digital Manometer	Yokogawa	2655	82DJ6001	Aug 06
Digital Manometer	Yokogawa	2655	82DJ6009	Aug 06

## ROUGH HANDLING TEST EQUIPMENT - Test sequences 3, 4, 5 & 6

<b>EQUIPMENT</b>	MANUFACTURER	MODEL	SN	CAL. DATE
Shock Amplifier	Endevco	2775A	ER34	NA
Shock Amplifier	Endevco	2775A	ER33	NA
Shock Amplifier	Endevco	2775A	EL81	NA
Item Accelerometer	Endevco	2228C	16471	Apr 06
Data Acquisition	GHI Systems	CAT	Ver. 2.7.1	N/A

**APPENDIX 5: Distribution List** 

### **DISTRIBUTION LIST**

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AFM C LSO/LO WRIGHT-PATTERSON AFB OH 45433-5540

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510 CBSS/GBM AD (ATTN THELMA LOOCK) 7973 UTILITY DRIVE BLDG 1135 HILL AFB UT 84056

586 CBSS/GBM CAA (ATTN WAYNE OSBORN) 375 PERRY STREET BLDG 255 ROBINS AFB GA 31098

658 AESS/LG (ATTN GERALD WILLIAMS) 2640 LOOP ROAD WEST WRIGHT-PATTERSON AFB OH 45433-5540

GENERAL ATOMICS ATTN DAVID LEVY 16761 VIA DEL CAMPO CT SAN DIEGO CA 92127 **APPENDIX 6: Report Documentation** 

REPORT DOCUMENTATION PAGE						Form Approved OMB No. 0704-0188
The public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, to Department of Defense, Washington Headquarters Services, Directorate for Information of perations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for felling to comply with a collection of information if it does not display a currently valid OMB control number.  PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.						
1. REPORT DATE (DD-MM-YYYY) 2. REPORT TYPE						3. DATES COVERED (From - To)
	·02-2008		Technical, Final Pro	ject Report	Es CON	March 06 - October 06
4. TITLE AND SUBTITLE 5a. CONTRACT NUMBER						
Development of the MQ-9 Reaper Propeller Container						
					5b. GRANT NUMBER	
					5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)					5d. PROJECT NUMBER	
Joel A. Sullivan, Project Engineer					06-P-105	
joel.sullivan@us.af.mil, DSN 787-8162, Comm. (937) 257-8162					5e. TASK NUMBER	
Susan J. Evans, Qualification Test Engineer					os. Men nemben	
susan.evans@us.af.mil, DSN 787-7445, Comm. (937) 257-7445					5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)						8. PERFORMING ORGANIZATION
Air Force Pack	kaging Techno	logy and Engi	neering Facility			REPORT NUMBER
AFMC LSO/LOP						08-R-02
5215 THURLOW ST, STE 5, BLDG 70C						
WRIGHT-PATTERSON AFB OH 45433-5540  9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)  10. SPONSOR/MONITOR'S ACRONYM(S)						
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)						10. SPONSOR/MONITOR S ACRONTINGS
					11. SPONSOR/MONITOR'S REPORT	
						NUMBER(S)
12. DISTRIBUTION/AVAILABILITY STATEMENT						
13. SUPPLEMENTARY NOTES						
14. ABSTRACT						
The Air Force Packaging Technology Engineering Facility (AFPTEF) was tasked with the design of a new shipping and storage container for the MQ-9 Reaper Propeller in March of 2006. The new container is designed to replace the fiberglass container currently used. The current container provides minimal shock protection and being fiberglass is susceptible to deformation, delamination, and extreme temperatures. Additionally, the fiberglass container can not house the propeller and spinner when the spinner is disassembled, the preferred shipping configuration. AFPTEF used proven design techniques to meet these design requirements. The CNU-690/E, designed to SAE ARP1967A, is an aluminum, long-life, controlled breathing, reusable shipping and storage container. The new container protects the Propeller mechanically and environmentally. The container passed all qualification tests per ASTM D4169. The CNU-690/E container not only meets user requirements but also provides an economic saving for the Air Force. The savings will be thousands of dollars per Propeller over the twenty-year life span of the container.						
15. SUBJECT TERMS						
CNU-690/E, MQ-9 Reaper Propeller Container, Aluminum Container, Reusable Container, Design, Test, Long Life						
16. SECURITY CLASSIFICATION OF: 17. LIMITATION OF 18. NUMBER 19a. NAME OF RESPONSIBLE PERSON						
a. REPORT b. ABSTRACT c. THIS PAGE ABSTRACT OF PAGES				OF PAGES	Joel A. Sullivan	
U	U	U	UU	38 19b. TELI		EPHONE NUMBER (Include area code) (937) 257-8162